



# Preparation and characterization of poly(acrylic acid)-hydroxyethyl cellulose graft copolymer

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## ABSTRACT

Poly(acrylic acid) hydroxyethyl cellulose [poly(AA)-HEC] graft copolymer was prepared by polymerizing acrylic acid (AA) with hydroxyethyl cellulose (HEC) using potassium bromate/thiourea dioxide (KBrO<sub>3</sub>/TUD) as redox initiation system. The polymerization reaction was carried out under a variety of conditions including concentrations of AA, KBrO<sub>3</sub> and TUD, material to liquor ratio and polymerization temperature. The polymerization reaction was monitored by withdrawing samples from the reaction medium and measuring the total conversion. The rheological properties of the poly(AA)-HEC graft copolymer were investigated. The total conversion and rheological properties of the graft copolymer depended on the ratio of KBrO<sub>3</sub> to TUD and on acrylic acid concentration as well as temperature and material to liquor ratio. Optimum conditions of the graft copolymer preparation were 30 mmol KBrO<sub>3</sub> and 30 mmol TUD/100 g HEC, 100% AA (based on weight of HEC), duration 2 h at temperature 50 °C using a material to liquor ratio of 1:10.

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## 1. Introduction

Synthesis of polyvinyl-polysaccharides composites has been investigated by a number of authors (Abdel-Halim, Abdel-Mohdy, et al., 2011; Abdel-Halim, El-Rafie, & Al-Deyab, 2011; Abdel-Halim, Emam, & El-Rafie, 2008; Chen et al., 2005; Hashem, Sokkar, Abdel-Halim, & Gamal, 2005; Joshi & Sinha, 2007). These composites have been synthesized to expand the market of polysaccharides-based products. These products are employed as reclaimable sizing agents (Hebeish, Higazy, El-Shafei, & Sharaf, 2010a; Mohamed, Amr, Knittel, & Schollmeyer, 2010) and substituent for the alginate thickener in the reactive printing (Gong et al., 2011; Turk & Schneider, 2000). Grafting of synthetic polymers onto biopolymers results in novel products having wide range of applications. This way of chemical modification yields new molecules with desirable properties of both biopolymer and synthetic polymer. Modern technologies require materials with precisely tuned properties by varying a set of parameters during synthesis, i.e. tailor-made materials (Abdel-Halim & Al-Deyab, 2011b; Abdel-Halim, Fahmy, & Fouda, 2008; El-Tahlawy, Abdel-Halim, Hudson, & Hebeish, 2007; Hebeish, El-Rafie, Abdel-Mohdy, Abdel-Halim,

& Emam, 2010; Ibrahim, Abdel Moneim, Abdel Halim, & Hosni, 2008; Sokkar, Abdel-Halim, Aly, & Hashem, 2004). Grafted polymers fit well in this category of materials as their properties can be precisely controlled by controlling the percentage grafting. Chemical grafting is one of the most effective methods of modifying structure and properties of biopolymers. Graft copolymerization of natural polysaccharides is becoming an important resource for developing advanced materials as it can improve the functional properties of natural polysaccharides (Ly, Bras, Sadocco, Belgacem, Dufresne, & Thielemans, 2010; Meshram, Patil, Mhaske, & Thorat, 2009; Rui-He, Wang, Wang, Yang, Zeng, & Ding, 2006; Szamel, Domjan, Klebert, & Pukanszky, 2008; Zhu, Dong, Wang, & Wang, 2010). The grafted polymers are usually synthesized by conventional redox grafting methods (da Silva, de Paula, & Feitosa, 2007; Hebeish, Abd El-Thalouth, El-Kashouti, & Abdel-Fattah, 2003; Kaith, Singha, & Kalia, 2007; Kang, Cai, & Liu, 2006; Singh, Tiwari, & Sanghi, 2005), by microwave irradiation (Masuhiro, Shafiu, Takayuki, Alessandra, & Giuliano, 2005; Singh, Tiwari, Pandey, & Singh, 2007), by  $\gamma$ -ray irradiation (Geresh, Gdalevsky, Gilboa, Voorspoels, Remon, & Kost, 2004; Wang, Chen, Zhang, & Yu, 2008) or by using electron beam (Vahdat, Bahrami, Ansari, & Ziaie, 2007).

Cellulose is the main constituent of cell wall in lignocellulosic plant, in which the cellulose content is 23–53% on a dry weight basis, less than that in cotton, which is almost made of pure fibrous cellulose (Knauf & Moniruzzaman, 2004). In the

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lignocellulosic materials, cellulose is embedded in a gel matrix composed of hemicelluloses, lignins, and other carbohydrate polymers (Hanley, Revol, Godbout, & Gray, 1997; Yu, Liu, Shen, Jiang, & Huang, 2005). The isolation of highly pure cellulose has been the subject of extensive studies for many years because of the complexity of cell wall structure (Brendel, Iannetta, & Stewart, 2000; Sun & Hughes, 1998). The use of cellulose obtained from sugarcane bagasse for production of cellulose derivatives has been reported in the literature (Gurgel, de Freitas, & Gil, 2008; Shaikh, Pandare, Nair, & Varma, 2009; Wang, Li, Xiao, & Wu, 2009). Also our research group has been working on demonstrating the viability of chemical recycling of cellulosic agricultural waste and industrial wastes for the production of higher value products (Abdel-Halim, 2012a, 2012b; Abdel-Halim, Abdel-Mohdy, Al-Deyab, & El-Newehy, 2010; Abdel-Halim & Al-Deyab, 2011a, 2011c, 2011d, 2012; Abdel-Halim, El-Rafie, & Kohler, 2008; Abdel-Halim, Fouda, Hamdy, Abdel-mohdy, & El-sawy, 2010; Abdel-Halim, Konczewicz, Zimmiewska, Al-Deyab, & El-Newehy, 2010a; Abdel-Mohdy, Abdel-Halim, Abu-Ayana, & El-Sawy, 2009; Fahmy & Abdel-Halim, 2010; Hashem, Abdel-Halim, El-Tahlawy, & Hebeish, 2005; Hashem, Abdel-Halim, & Sokker, 2007; Hebeish, Ramadan, Abdel-Halim, & Abo-Okeil, 2011). Few commercial uses for the excess bagasse have been developed and its accumulation presents a waste problem for the sugar industry. The same is the case with wheat and rice straw, cereal straws, cotton stalks, etc. One area where tremendous amount of research has been devoted pertains to the fractionation of agricultural biomass into its constituents, i.e. cellulose, hemicellulose, and lignin in what is best described as a bio-refinery. Each of these fractions can then be separately value-added by making industrially important derivatives. For example, cellulose can be converted into cellulose esters (Shaikh et al., 2009), which have wide ranging applications as biodegradable plastics, textile fibers, films, etc. and cellulose ethers (Vieira et al., 2009) which find many industrial applications as thickeners.

Hydroxyethyl cellulose (HEC) is a nonionic, water-soluble polymer that can thicken, suspend, bind, emulsify, form films, stabilize, disperse, retain water, and provide protective colloid action. It is readily soluble in hot or cold water and can be used to prepare solutions with a wide range of viscosities. Hydroxyethyl cellulose has many industrial applications like contributing a desired body in paints (Dal-Bó, Laus, Felipe, Zanette, & Minatti, 2011), textile finishing (Gorgieva & Kokol, 2011), thickening cement mortar (Patural, Marchal, Govin, Grosseau, Ruot, & Devès, 2011) and paper making (Kugge, Craig, & Daicic, 2004). In the manufacture of hydroxyethyl cellulose, purified cellulose is reacted with sodium hydroxide to produce swollen alkali cellulose. This alkali-treated cellulose is more chemically reactive than cellulose. By reacting the alkali cellulose with ethylene oxide, a series of hydroxyethyl cellulose ethers is produced. In this reaction, the hydrogen atoms in the hydroxyl groups of cellulose are replaced by hydroxyethyl groups, which confer water solubility to the product when the molar substitution reaches certain value.

Recently we have studied the conversion of sugarcane bagasse cellulose to valuable products, hydroxyethyl cellulose (HEC). To fulfill more industrial application to the HEC obtained from the purified sugarcane bagasse, we use it in the current study as a starting material for preparation of poly(AA)-HEC composite. The composite is a term given to the reaction product of the HEC, the acrylic acid (AA) and the initiator when all these ingredients are present in aqueous system for polymerization. Based on that, the present study is concerned with polymerization of acrylic acid with hydroxyethyl cellulose using  $\text{KBrO}_3$ -TUD redox system. The polymerization reaction will be carried out under different conditions including concentration of AA,  $\text{KBrO}_3$ , TUD, material to liquor ratio and temperature of polymerization.

## 2. Experimental

### 2.1. Materials

#### 2.1.1. Cellulosic raw material

Fresh bagasse was washed thoroughly in running water to make sure that all sugar residues were washed off to minimize microbial attack. The washed bagasse was dried in sunny area until it is completely dry and then ground into fine particles using Fritsch mill, Type 15.302 (Germany). The ground bagasse was subjected to alkali treatment followed by bleaching with sodium chlorite activated with hexamethylenetetramine (Abdel-Halim, 2012b). The so bleached ground bagasse was used as a starting material for the preparation of hydroxyethyl cellulose, according to a reported method (Zahran, Abdel-Halim, & El-Rafie, 1998).

#### 2.1.2. Chemicals

Acrylic acid (AA) potassium bromate, thiourea dioxide (TUD), sulphuric acid, sodium thiosulphate, potassium iodide, and potassium bromide were laboratory grade reagents.

### 2.2. Preparation of poly(AA)-HEC composite

Hydroxyethyl cellulose dissolved in water was stirred well and the temperature was raised to the desired polymerization temperature. When the desired reaction temperature was attained, known concentrations of acrylic acid and aqueous solution of the initiation components (potassium bromate/thiourea dioxide) were added to the hydroxyethyl cellulose solution. A material to liquor ratio of 1:10 was employed and the reaction was allowed to proceed under continuous stirring for 120 min.

### 2.3. Testing and analysis

#### 2.3.1. Total conversion

The percentage total conversion was calculated by quantitative estimation of the acrylic acid double bonds, according to a reported method (Sailaja & Murthy, 2010).

#### 2.3.2. Apparent viscosity

The apparent viscosity of the poly(AA)-HEC composite was evaluated using Bohlin Rotational Viscometer at different rates of shear.

## 3. Results and discussion

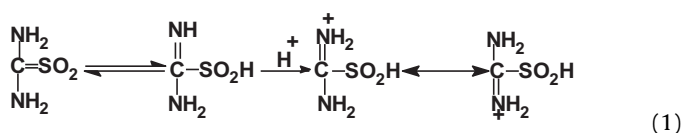
### 3.1. Preparation of poly(AA)-HEC graft copolymer

The synthesis of poly(AA)-HEC graft copolymer was achieved using a very efficient potassium bromate-thiourea dioxide redox initiation system. Effect of the concentrations of  $\text{KBrO}_3$ , TUD and AA, the material to liquor ratio, the polymerization temperature and polymerization duration were studied. However, before going into detailed investigation of these parameters, it seems logical to shed some insight on the mechanisms involved in the polymerization reaction using the aforementioned initiation system.

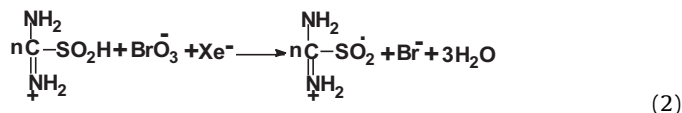
### 3.2. Tentative mechanism

When potassium bromate (oxidant) is coupled with thiourea dioxide (reductant), in acidic medium, a very efficient redox system is established. In the presence of AA as a monomer and hydroxyethyl cellulose which contains functional hydroxyl groups in the cellulose structure and the terminal hydroxyethyl group, the primary free radical species brought about by decomposition of the redox system can initiate homopolymerization of AA as well as

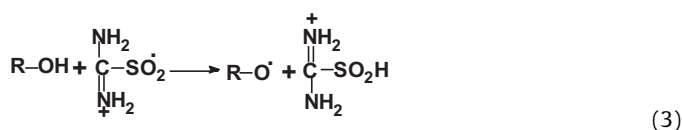
grafting of the latter onto the HEC molecules. Specifically the polymerization process involves conversion of thiourea dioxide, in acidic medium, to isothiurea dioxide (Eq. (1)).



Isothiurea dioxide reacts with bromate anion to generate isothiurea dioxide free radicals (Eq. (2)).

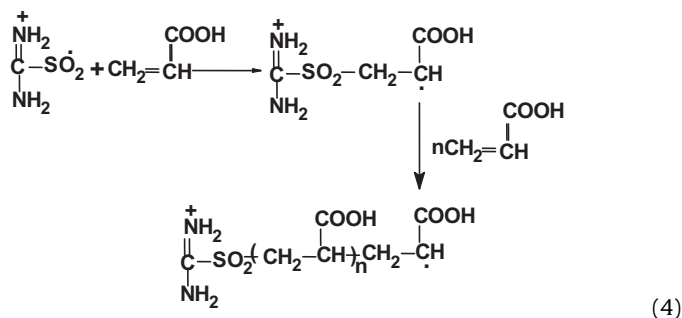


The isothiurea dioxide radicals attack functional hydroxyl groups of HEC to form HEC free radicals (Eq. (3)).

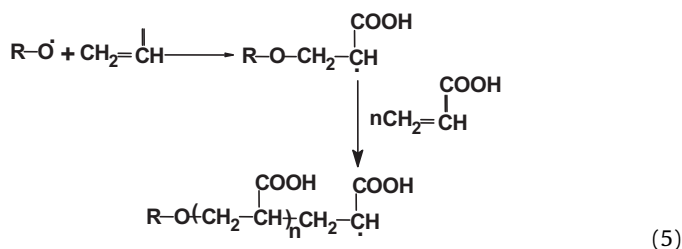


where R-OH = Cell-OH or Cell-O-CH<sub>2</sub>CH<sub>2</sub>-OH.

Furthermore, isothiurea dioxide can strongly initiate homopolymerization of AA molecules (Eq. (4)).



The reaction of hydroxyethyl cellulose free radical with AA initiates the grafting reaction along the HEC backbone (Eq. (5)).



It should be mentioned that KBrO<sub>3</sub> plays an important role other than initiation of AA polymerization, namely oxidation of HEC molecules, particularly at higher bromate concentration. Furthermore, the Br<sub>2</sub> molecules liberated at higher bromate concentration may also attack and oxidize the HEC with subsequent degradation of HEC molecules (Eq. (6)).



Taking the above tentative mechanisms into consideration, the factors affecting the preparation of the poly(AA)-HEC composite were studied. The results obtained are given below along with their appropriate discussion.

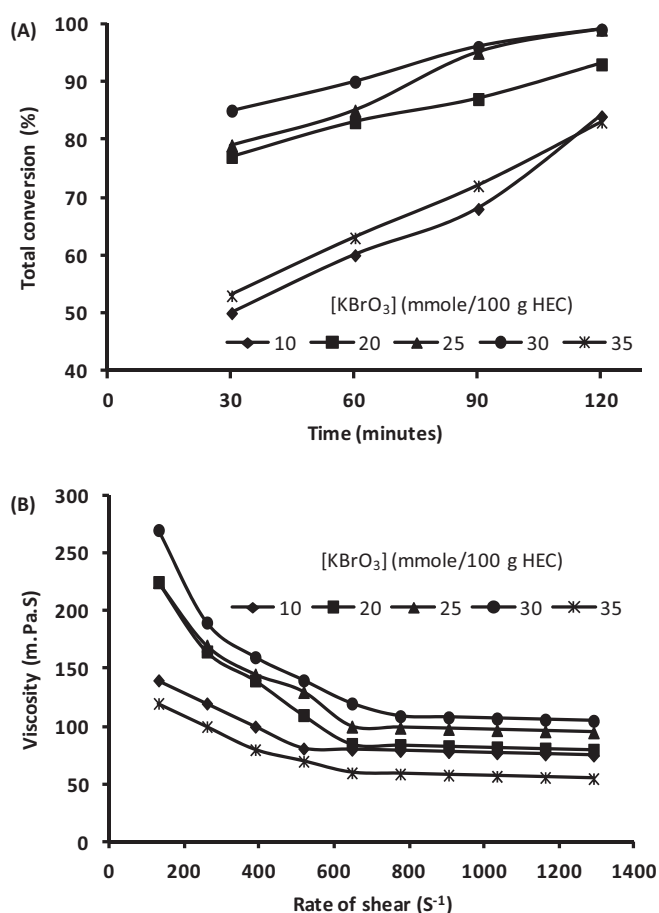


Fig. 1. Effects of KBrO<sub>3</sub> concentration on: (A) total conversion and (B) viscosity.

### 3.3. Effect of initiator components concentrations

#### 3.3.1. Potassium bromate concentration

Fig. 1A shows the dependence of the extent and rate of polymerization of acrylic acid, expressed as percent total conversion, on KBrO<sub>3</sub> (oxidant) concentration. It is observed (Fig. 1) that, regardless of the used KBrO<sub>3</sub> concentration, the total conversion is characterized by an initial fast rate followed by a slower rate. It is obvious that the total conversion increases with the increase in KBrO<sub>3</sub> concentration up to 30 mmol/100 g HEC and decreases significantly with further increase in KBrO<sub>3</sub> concentration. Enhancement of acrylic acid conversion to poly(acrylic acid) could be interpreted in terms of the redox process under question. The data indicate that maximum total conversion is attained at equimolar ratio of KBrO<sub>3</sub> and TUD 30:30 mmol/100 g HEC. The enhancement in the polymerization reaction at this critical concentration could be explained in terms of creation of larger amounts of free radicals (Eqs. (2)–(4)). Inhibition of the polymerization reactions by liberated Br<sub>2</sub> (Eq. (6)) as well as participation of the bromate ion at higher concentrations in the termination process may explain the lowering of the total conversion of AA when KBrO<sub>3</sub> concentration higher than 30 mmol/100 g HEC was used.

Fig. 1B shows the effect of KBrO<sub>3</sub> concentration used during the polymerization on the apparent viscosity of the resultant composite paste (5% solid content) measured at different shear rates. It is seen that, regardless of the KBrO<sub>3</sub> concentration used, the apparent viscosity decreases significantly by increasing the shear rate

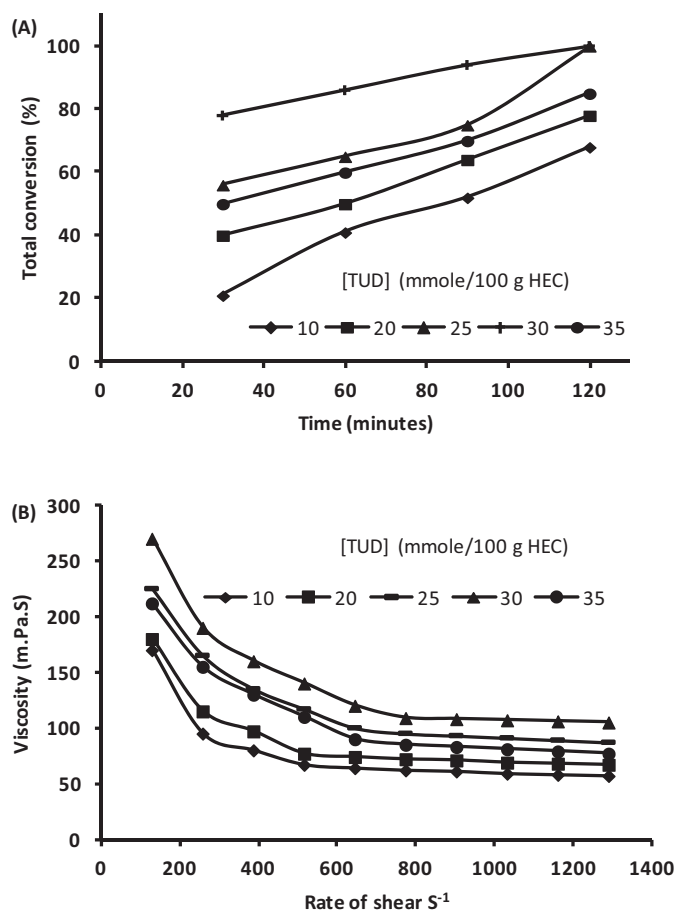


Fig. 2. Effects of TUD concentration on: (A) total conversion and (B) viscosity.

up to  $774 S^{-1}$  then levels off beyond this limit. It is clear also that the apparent viscosity of the composite is lower than that of HEC. The data (Fig. 1B) indicates that the apparent viscosity decreases by increasing  $KBrO_3$  concentration. This behavior could be ascribed to the degradative effect of  $KBrO_3$  on HEC molecule and the degradation of HEC by  $Br_2$  molecules liberated at higher  $KBrO_3$  concentrations (Eq. (6)), in addition to the lower total conversion at higher  $KBrO_3$  concentration.

### 3.3.2. Thiourea dioxide concentration

Fig. 2A shows the effect of TUD concentration on the extent and rate of AA polymerization. The polymerization reaction was carried out at  $50^\circ C$  for 2 h, using 30 mmol  $KBrO_3$ /100 g HEC, 100 g AA/100 g HEC, material to liquor ratio 1:10, and 10–35 mmol TUD/100 g HEC. It is seen that, the total conversion of AA to poly(AA) increases by increasing TUD concentration up to 30 mmol/100 g HEC. Further increase in TUD concentration beyond this limit is accompanied by significant decrease in the total conversion.

This behavior indicates that maximum polymerization is obtained when equimolar ratio of both the oxidant and the reductant were used (i.e.  $KBrO_3$ :TUD is 30:30 mmol/100 g HEC) and this confirms the results obtained above. Increase in the formation of active species (isothiurea dioxide free radicals) may account for the enhancement in the polymerization reaction by increasing TUD concentration up to 30 mmol/100 g HEC. However, by further increasing TUD concentration, the concentration of isothiurea dioxide free radicals is increased to such an extent that they tend to homocombine to give inactive species, rather than to initiate

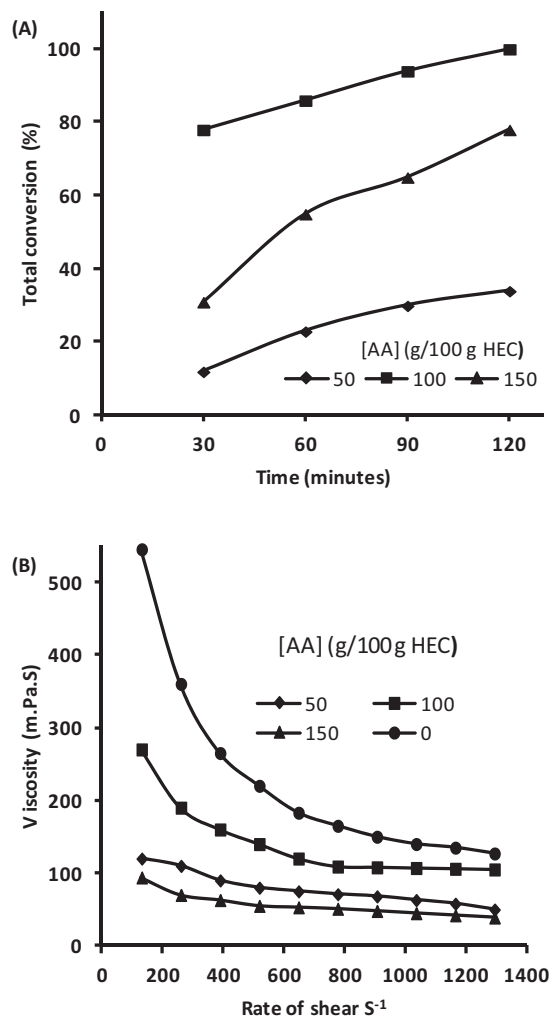
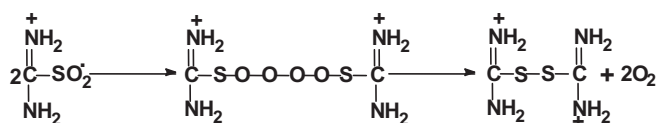


Fig. 3. Effects of acrylic acid concentration on: (A) total conversion and (B) viscosity.

polymerization of AA (Eq. (7)).



(7)

Fig. 2B shows the dependence of the apparent viscosity of the composite paste (5% solid content) on the concentration of TUD used for the polymerization reaction. The results reveal that the viscosity decreases with increasing TUD concentration within range studied. The degradation of the HEC chains due to the effect of the initiation components and the formation of low molecular weight fragments leads to the decrease in the composite viscosity.

### 3.3.3. Acrylic acid concentration

Fig. 3A shows the relationship between the total conversion percentage and polymerization time when different amounts of acrylic acid were incorporated in the polymerization medium (50%, 100% and 150% based on weight of HEC). The results reveal that, increasing AA concentration from 50% to 100% based on weight of HEC is accompanied by a substantial enhancement in the extent and rate of polymerization. Further increase in AA concentration up to 150% leads to a significant decrease in the extent and rate of polymerization. Enhancement of the polymerization rate is attributed

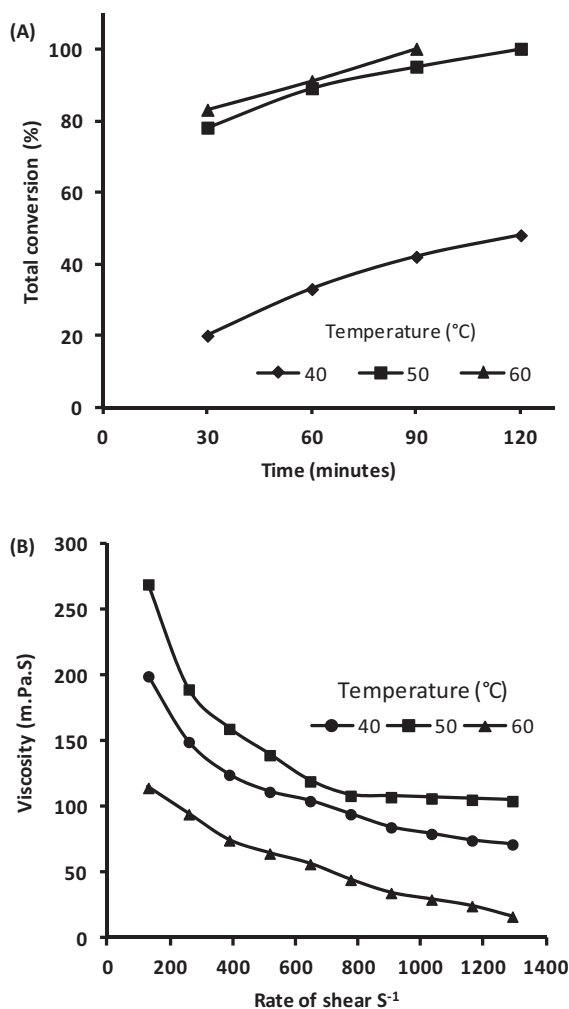


Fig. 4. Effects of polymerization temperature on: (A) total conversion and (B) viscosity.

to the increase in acidity of the polymerization medium as the AA concentration increases. This brings about improvement in  $KBrO_3$  efficiency as an oxidizing agent and stabilization of the formation of isothiourea dioxide via the excessive protons present in the polymerization medium (Eq. (1)), this in addition to enhancement of the redox process as a whole. The decrement in the extent and rate of polymerization on using 150% AA may be attributed to shortage in the active species which initiate this amount of AA. Furthermore, liberation of  $Br_2$  at this highly acidic medium leads to oxidation reaction rather than polymerization reaction.

Fig. 3B shows the apparent viscosity of the poly(AA)-HEC composite paste prepared using different AA concentrations as a function of rate of shear. It is evident that the apparent viscosity of the prepared composite is lower than that of the blank HEC. The apparent viscosity of the prepared composites follows the order:

$$100\% \text{ AA} > 50\% \text{ AA} > 150\% \text{ AA}.$$

This behavior reflects the effect of the redox system and the acidity of the polymerization medium on the chain length of the poly(AA) (homopolymer and grafted chains) and HEC.

### 3.3.4. Polymerization temperature

Fig. 4A shows the effect of temperature on the extent and rate of AA polymerization. Monitoring the total conversion of AA during the polymerization reaction shows it to be temperature dependent,

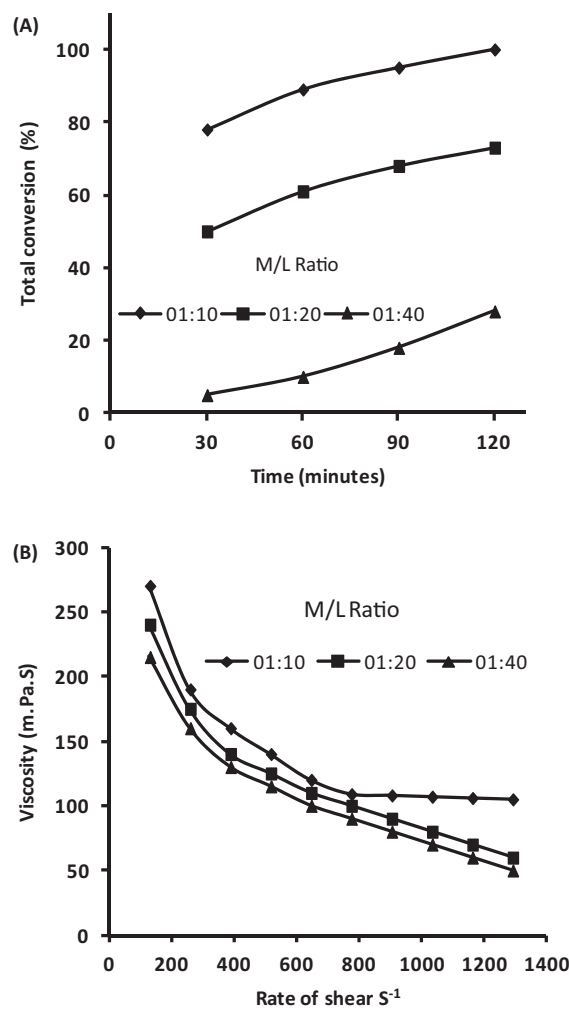


Fig. 5. Effects of material to liquor ratio on: (A) total conversion and (B) viscosity.

following the order:  $60^\circ\text{C} > 50^\circ\text{C} > 40^\circ\text{C}$ . This could be interpreted in terms of the favorable influence of temperature on the efficiency of the redox process, the kinetic energy and diffusibility of AA molecules and/or radicals and the number of collisions between the monomer radicals and monomer molecules.

Fig. 4B demonstrates the influence of the polymerization temperature on the apparent viscosity of the resultant composite paste. The data indicates that apparent viscosity depends on the polymerization temperature and follows the order:  $50^\circ\text{C} > 40^\circ\text{C} > 60^\circ\text{C}$ . The lower viscosity at  $60^\circ\text{C}$  is ascribed to higher rate of termination which leads to shorter poly(AA) chains and the degradative effect of the redox system at high temperatures.

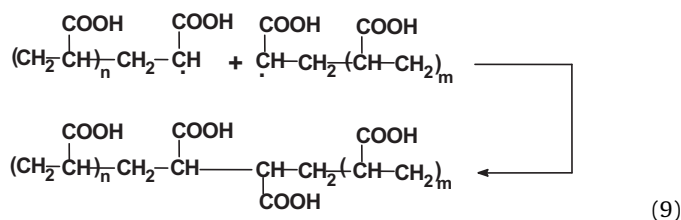
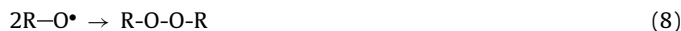
### 3.3.5. Material to liquor ratio

Fig. 5A shows the effect of material to liquor ratio (M/L ratio) on the extent and rate of AA polymerization with HEC. It is seen that the extent of polymerization depends on the ratio of HEC to the volume of the polymerization medium and follows the order:  $1:10 > 1:20 > 1:40$ . Obviously, the extent of polymerization decreases by increasing the liquor ratio. This could be attributed to the dilution of the reactants in the reaction medium. Dilution reduces molecular collision and, therefore, the opportunity of the molecules of the reactants to undergo polymerization reaction.

Fig. 5B shows the effect of M/L ratio on the apparent viscosity of the resultant poly(AA)-HEC composite paste measured at different rates of shear. It is clear that the apparent viscosity of the composite prepared at lower liquor ratio of 1:10 is higher than that of the



prepared at higher liquor ratios of 1:20 and 1:40. It seems logical that using lower liquor ratio establishes rapid combinations between chains of HEC radicals ( $R-O^\bullet$ ) and poly(AA) radicals (Eqs. (8) and (9)).



This chains lengthening is responsible for the increased viscosity at lower liquor ratio.

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